

MARINE ENVIRONMENT PROTECTION COMMITTEE 74th session Agenda item 17

MEPC 74/INF.28 8 March 2019 ENGLISH ONLY

ANY OTHER BUSINESS

Ship underwater radiated noise technical report and matrix

Submitted by Canada

SUMMARY									
Executive summary:	This document highlights the results of a recent review of underwater radiated noise mitigation measures from ships. These options are presented as a matrix, focussing on new builds and retrofit technologies.								
Strategic direction, if applicable:	4								
Output:	Not applicable								
Action to be taken:	Paragraph 4								
Related documents:	MEPC 71/16/5; MEPC 72/16/5; MEPC 73/18/4, MEPC 73/INF.23; MEPC 74/17/2 and MEPC 74/INF.36								

1 In order to further understanding and develop measures surrounding underwater radiated noise (URN) from ships, Canada commissioned Vard Marine, Inc. (a Fincantieri Company) to prepare a report that reviews the means of mitigating and predicting the URN from ships. The main outcome of the report is a technical matrix of options and aspects, which can be used as a stand-alone summary of URN reduction measures applicable now and in the future.

2 Attached in the annex are key excerpts from the report, including the executive summary, the URN matrix, and citations.

3 IMO Member States, intergovernmental, and non-governmental organizations interested in reviewing the full report, which includes a summary of URN sources and its effects on marine life, as well as the methodology for the matrix, can request a copy through Transport Canada at: TC.QuietShips-Naviressilencieux.TC@tc.gc.ca.

Action requested of the Committee

4 The Committee is invited to note the information provided in this document.



ANNEX

EXCERPTS FROM THE REPORT "SHIP UNDERWATER RADIATED NOISE", PREPARED BY VARD MARINE INC FOR TRANSPORT CANADA (FEBRUARY 2019)

Executive Summary

1 This report presents the results of a review of means of mitigating and predicting the underwater radiated noise (URN) from ships. This noise can have significant environmental impacts, with damaging effects on marine animals of many types. The report provides an overview of URN issues but is not intended as a complete guide to this very complex subject.

2 The main outcome of the work undertaken is a matrix of URN mitigation measures, presented as appendix 1 to the report, which can be used as a stand-alone summary of options that can be used now and in the future. Measures are categorized in four main areas:

- .1 propeller noise reduction;
- .2 machinery noise reduction;
- .3 flow noise reduction; and
- .4 other, where the first three categories are not easily applied.

3 Each measure is described, and then defined in a standardized approach that aims to define:

- .1 advantages and benefits to the ship's design and operations;
- .2 disadvantages and challenges;
- .3 technology readiness;
- .4 cost impacts for implementation and operation;
- .5 applicability to different ship types; and
- .6 effectiveness; in terms of frequency ranges and reduction in sound levels.
- 4 A final section of the matrix provides a summary of prediction methods for URN.

5 Entries in the matrix are supported by citations, and a full list of references is provided in appendix 2 to the report.

6 A wide range of mitigation measures are available to address different types of noise at varying levels of effectiveness. All will incur some level of cost, but in some cases there are co-benefits such as efficiency enhancements that may offset some or all of this disadvantage.

APPENDIX 1

MATRIX OF URN MITIGATION MEASURES

Underwater Radiated Noise Matrix Terminology

Advantages/Benefits

- Enhanced Crew/passenger Comfort CC -
- Е Reduced Emissions
- Enhanced eFficiency F -
- **Reduced Maintenance** Μ -
- Increased MAneuverability MA -
- S Decreased Space Demand -
- Decrease in Weight W -

Disadvantages/Challenges

- D Increased Design effort -
- Increased Emissions Е -
- F Reduced eFficiency
- Increased Maintenance Μ -
- Reduction in MAneuverability MA
- Increased complexity Ρ -
- Increased Space demand S -
- W Increased Weight -

TRL - Technology Readiness Level

Cost Estimation

Range	-	Range of expected cost
Percentage	-	Percentage increase or decrease
Payback Period	-	Time in months/years to recover
investment		
Shorthand	-	Whether to expect an increase or
decrease		
Technology Mat	rix	

Applicability ReFit

New Build

-

-

- RF NB
- Ship Type
- By quadrant from Figure, except where indicated

4			Larger			1
	Tanl	kers 🕴				
	Bulk Carrie	ers			Contain	er Ships
				LNG C	arriers	
	Ferries				Cruise S	hips
			Ve	ehicle Carri	ers	
Slower						Faster
	Ferries					
	Offsho	re			Wars	hips
	Supply	Vessels				
				Ferries		
	Fishing Ves	sels	Crewb	oats		
	Tugboats					
3			Smaller			2

Effect

Frequency Range - Broadband/Narrowband; Expected Frequency Range Affected in Hertz (Hz) Noise Reduction - Expected Noise Reduction in Decibels (dB): Low (up to 5 dB), Medium (5-10 dB), High (greater than 10 dB)

Treatment/Description	Advantage s/Benefits	Disadvantage s/Challenges	TRL	Cost Estimation Percentage/	Applicability RF/ NB	Effect Frequency	Effect Noise
				Range	Ship Types	Range (Hz)	Reduction (dB)
1. PROPELLER NOISE							
1.1 PROPELLER/PROPULSOR DESIGN							
1.1.1 Reduction of Turns per Knot (TPK): Reducing the number of propellers turns per knot of speed, thus, reducing the speed of the flow at the tips of the blades. This requires a larger diameter of propeller and is applicable to both fixed and control pitched propellers. Reduces all forms of propeller cavitation (especially propeller tip cavitation) and increases Cavitation Inception Speed (CIS).	F CC	D	9	Unknown	NB 1 - 4	ALL	Dependent on application – low to medium
1.1.2 Increased Propeller Immersion: The hydrostatic pressure put forth on the propeller can affect the amount of cavitation that occurs and the CIS. The greater distance the propeller is from the free surface of the sea, the less cavitation will occur and the higher the CIS. Practical design constraints may limit. [2]		D	9	Unknown	NB 1 – 2	Unknown	Low
1.1.3 High Skew Propeller: Propeller with blades swept back substantially more than conventional propellers. This allows for the blade to pass through the varying wake filed in a more gradual manner, improving the cavitation patterns. Load reduction on the tip of the propeller results in further reduction of propeller cavitation and increased Cavitation Inception Speed (CIS). [3] [4] [5]	F CC M	D F W	9	10-15% Higher capital cost than conventional propellers	RF/ NB 1 - 2	40-300	Medium, depending on initial wake field
1.1.4 Contracted Loaded Tip Propellers (CLT): Propellers designed with an end plate allowing for maximum load at the propeller tip, which reduces propeller tip cavitation and increases CIS. The end plate also promotes a higher value of thrust per area (higher speed with smaller optimum diameter) further reducing noise, vibrations and further increasing Cavitation Inception Speed (CIS). [5] [6] [7]	F CC	D	9	20% Higher capital cost than conventional propellers	RF/ NB 1 – 4	40-300	Medium
1.1.5 Contra-rotating Propellers: Co-axial propellers, one propeller rotating clockwise & the other rotating counter clockwise. Increases CIS due to reduction in blade loading resulting in lower blade surface cavitation. Also, optimised flow circulation results in lower tip vortex cavitation. [8] [9]	F	D M P	9	Much higher capital cost than conventional propellers	RF/ NB 1 – 2	40-300	Low to medium

Treatment/Description	Advantage s/Benefits	Disadvantage s/Challenges	TRL	Cost Estimation Percentage/	Applicability RF/ NB	Effect Frequency	Effect Noise
1.1.6 Kappel Propellers: Propeller blades modified with tips curved towards the suction side. This reduces the strength of the tip vortex thus increasing efficiency, decreasing tip vortex cavitation, and increasing CIS. [10] [11]	F	D	9	20% higher capital cost than conventional propellers [5]	RF/ NB 1 – 2	40-300	Low
1.1.7 Propeller with Backward Tip Raked Fin: Propeller modified in such a way the blades are curved towards the Pressure side (Opposite of Kappel Propellers), Studies have shown that there is an increase in efficiency and decrease in cavitation expected, however, there are few studies on the subject. [12]	F	D	6 9	Higher capital cost than conventional propellers	RF/ NB 1 - 2	Unknown	Unknown (Improves wake flow)
1.1.8 Podded Propulsors: This type of propulsion achieves improved wake performance to the propeller reducing cavitation and CIS. However, the drive configuration can increase medium to high frequency noise; see also 2.2.1 (Enabled by Diesel electric design) [13] [14]	CC MA	D P F	9	Power dependent; typically 25% more than shafted system	NB 1 – 4	Unknown	Low to Medium
1.1.9 Water Jets: Operate in ducting internal to the ship, with increased pressures at the jet. Noise reduction from higher cavitation inception speed and by isolating the propeller from the sea. [14] [15] [16]	F (high speed) high power density for fast, shallow draft vessels	F (at low speeds) M P W	9	Higher than conventional propeller and shafting; higher installation cost	NB 2 Highest speeds and some speciality types	All	High
1.1.10 Pump Jets: Combine a full pre-swirl stator, propeller and duct. Used in ultra- quiet applications such as submarines. [17]		F M P W	7 (for conven tional ships)	Higher cost than conventional prop	NB 2	All	High
1.1.11 Composite Propellers: Use of advanced composites to allow for blade (tip) distortion under load to delay cavitation onset and reduce blade vibration.	CC W	D	6	Unknown at this time	NB/RF 2, 3	All	Low
1.2 WAKE FLOW MODIFICATION	_	-					
1.2.1 Pre-swirl Stator: Consists of Stator blades located on the stern boss in front of the propeller, flow is redirected before entering the propeller, increasing over all flow performance, thus reducing cavitation and increases CIS. [17]	F	D	9	Typical Payback Period: 24 months	RF/ NB 4	All	Low

Treatment/Description	Advantage	Disadvantage	TRL	Cost Estimation	Applicability	Effect	Effect
	s/Benefits	s/Challenges		Percentage/	RF/ NB	Frequency	Noise
				Range	Ship Types	Range (Hz)	Reduction (dB)
1.2.2 Schneekluth Duct:	E-	D	9	Typical	RF/NB	All	Low
An oval shaped duct located just forward of the upper half of the	F			Payback Period:	1, 4		
propeller, designed to improve the flow to the upper part of the				4 months			
propeller, this improves flow performance, lowering the formation of							
cavitation of propeller blade tips and increasing CIS. [18] [19]							
1.2.3 Propeller Boss Cap Fin (PBCF):	E	D	9	Typical Payback	RF/NB	≤ 1.0kHz	Medium
Small fins attached to the hub of the propeller, reducing hub vortex	F			Period:	1, 4		
cavitation, thus, reducing noise and vibration and increasing CIS.				4 – 6 months			
The design also recovers lost rotational energy, increasing				[21]			
efficiency. Similar concepts include ECO-CAP [19] [20]							
1.2.4 Propeller Cap Turbines (PCT):	E	D	9	Typical Payback	RF/NB	≤ 1.0kHz	Medium
Hydrofoil shaped blades integrated into the hub cap, similarly to	F			Period:	1, 2, 4		
PBCF reducing hub vortex cavitation, and increasing CIS. The				4 – 6 months			
design also recovers lost rotational energy, increasing efficiency.				[22]			
[19] [20]							
1.2.5 Grothues Spoilers	E	D	9	Typical Payback	RF/NB	Unknown	Low
A small series of curved fins attached to the hull forward of the	F			period:	1, 4		
propeller, designed to improve flow to the propeller, reducing				Less than a year			
cavitation, increasing CIS and increasing fuel efficiency. [18]							
1.2.6 Mewis Duct	E	D	9	Typical Payback	RF/NB	Unknown	Low
A combination of a duct with pre-swirl stators integrated into the duct	F			Period:	1, 4		
just forward of the propeller, thus having the benefits of both pre-				Less than a year			
swirl stators and grothues spoiler. Similar concepts include Super							
Stream Duct [5] [23]	_	-	-				-
1.2.7 Promas:	F	D	9	Typical Payback	NB	Unknown	Low to
Integration of the propeller, hubcap, rudder bulb, and rudder into one	E			Period: less than	1, 2		Medium
hydrodynamic efficient unit. Reduces propeller tip loading and				2 years			(depending on
limiting blade pressure pulses, thus, reducing cavitation and CIS.							initial flow)
Similar concepts include Ultimate Rudder Bulb and SURF BULB[24]	-				10/05	<u></u>	
1.2.8 Costa Propulsion Bulb (CPB):	F	D	9	Payback Period:	NB/ RF	Unknown	Low
Consists of two bulb halves that are welded to the rudder, in line with				4 – 15 years	1, 2		
the propeller. Designed to recover energy losses att of the propeller,				[22]			
by eliminating vortices caused by cavitation, ultimately reducing							
propeller vibrations and lowering URN. [25]		_	•				•
1.2.9 I WISTER KURRET:		ט	9	Payback Period:	NB/ RF	Unknown	LOW
Rudder designed to twist in order to vary the angle of attack to match				4 – 15 years	1, Z		
water flow pattern. This reduces all cavitation and increases CIS. Used	WA			[22]			
on a variety of vessels, including BC Ferries and U.S Navy Destroyers.				[22]			
[20]							

Treatment/Description	Advantage s/Benefits	Disadvantage s/Challenges	TRL	Cost Estimation Percentage/ Range	Applicability RF/ NB Ship Types	Effect Frequency Range (Hz)	Effect Noise Reduction (dB)
1.2.10 Asymmetric Body for Single Screw Vessels The purpose of designing an asymmetric after body is to account for the asymmetrical flow of a single screw propeller about the centerline. This will slightly increase CIS. [27] [3]	F	D	9	Unknown	NB 1, 4	Unknown	Low
1.2.11 CPP Combinator Optimization Adjusting pitch and rpm settings for controllable pitch propellers can mitigate the early onset of cavitation on pressure and suction sides both at constant speeds and during acceleration. This may also improve propeller efficiency in these conditions [77]	F	D	8	Modest, requires software updates and potentially additional sensors	NB/RF All	All	Medium
1.3 SUPPLEMENTARY TREATMENTS	_	_	-				-
1.3.1 Improved Manufacturing Processes: Tighter tolerances on blade manufacture may reduce cavitation. [28]	F	D	9	10+% more expensive than standard propeller	NB/RF 1 - 4	Unknown	Low
1.3.2 Air Bubbler System (Prairie): Air injection through holes in the propeller blade tips, this fills the vacuum left by the cavitation as propellers rotate, allowing cavitation bubbles to contract more slowly as area that is under pressured is minimised. Reducing cavitation and increasing CIS. Must be used while docked as well to reduce marine growth clogging holes. Used by navies to reduce noise for stealth purposes. [29]		D F M	6 (in comm ercial applic ation)	20000 – 75000 +	NB 1, 2	20 – 80 500+	Medium
1.3.3 Propeller Blade maintenance Imperfections of a propeller blade can encourage cavitation. Polishing between dry docks can prevent this, reducing cavitation and increasing CIS. [30]	F	М	9	Unknown	RF 1 - 4	All	Low
1.3.4 Anti-Fouling Coating: A coating applied to the surface of a propeller with the purpose of reducing propeller fouling. Research has been done regarding underwater noise with varying results. [31]	M		9	Payback Period: 2 years [22]	NB/RF All	50 -10000Hz	Low
1.3.5 Application of Anti-Singing Edge: Modification to the propellers trailing edge, designed to alter naturally occurring vortex shedding phenomenon. [32] [33]			9	Increase in manufacture cost	NB/RF 1 - 4	10 – 12000	High (where singing is a problem)

Treatment/Description	Advantage	Disadvantage	TRL	Cost Estimation	Applicability	Effect	Effect
	S/Benefits	s/Challenges		Percentage/	RF/ NB Shin Typos	Frequency	NOISE Reduction (dR)
2.0 MACHINERY				Range	Ship Types	Italige (IIZ)	Reduction (db)
2.1 Machinery Selection							
2.1.1 Prime Mover Selection							
The choice of prime mover (main engines) has a strong influence on							
the basic machinery noise characteristics of the ship and on the							
potential use of mitigation measures. Diesels are currently the							
default choice of prime mover for almost all commercial vessels and							
so are assumed here except where otherwise indicated. See main							
report for additional discussion.		-			ND		
2.1.2 (Diesei) Electric:	MA (paired	F	9	Highly variable	NB	ALL	High
facilitates many paice reduction approaches from the use of mounts	with				MOSt applicable to		
and enclosures to active noise cancellation. A wider range of	thrusters)				vessels that		
propulsor selections are also available. Electrical transmission has	S				have widely		
worse efficiency than mechanical, and capital costs are higher so	W				varying		
use is generally in vessels where other benefits outweigh these					speeds in		
costs. [34]					operational		
					profile, and/or		
					redundancy		
					requirements		
					for dynamic		
					etc		
2.1.3 Gas/Steam Turbine	S	F	9	Much higher	NB	ALL	High
Rotating turbines are generally quieter than diesels but have lower	CC	D		capital cost than	1, 2		
fuel efficiency and higher capital cost. Very few steam ships are now	E	Μ		diesel			
constructed (other than for nuclear vessels) but many naval vessels	(compared	Р					
use gas turbines for high power density. [35]	to Diesel)	14/	0	Illink constations of	ND		Maallaana
2.1.4 Stirling Engine:	F	W S	6	High capital cost	NB	Unknown	Medium
I ne external compustion stirling engine produces lower noise then	E (multiplo	3					
conventional internal compusion engines. Load following	fuel						
of power. Main uses are for submarines and naval vessels to reduce	capability)						
radiated noise.	M						
[36]							
2.1.5 Azimuthing Propulsors	F	F (compared	9	Power	NB	Unknown	Unknown
Azimuthing propulsors may have motors inside the hull with	(compared	to		dependent;	1, 2, 3		
transmission gears (electro-mechanical) or outside the hull in a	to			typically 25%			

Ireatment/Description Advantage Disadvantage IRL Cost Estimation Applicability Effect Effect	π
S/Denems S/Chailenges Percentage/ RF/NB Frequency Noise	
Range Ship Types Range (T2) Reduction	(UD)
bonofite on poted in 1.1.9. Electro mochanical types may have goor and discal discal discal discal	
beine to mitigate while fully electric have electric here a lectric le	
Limited public domain information is available on the machinery MA	
Inited public domain monitation is available on the machinely machine characteristics of either type though both claim excellent W	
2.2 Machinery Treatments	
2.2.1 Resilient Mounts (Equipment): CC S 9 20 – 2000\$ per NB/ RF All High, ber	stat
Spring mounts impede the transmission of vibration energy from W mount: large 2.3	er er
machinery, and the generation of energy into the water from the hull.	cies
Requires appropriate selection and installation of mounts. Not many mounts	
generally practical for heavy 2-speed diesels. and installation	
[37] cost,	
2.2.2 Floating Floor (Deck): CC S 9 Unknown NB/ RF All Low, ma	ain
A Floating/False deck is constructed and resiliently mounted to the W All benefit	its
deck, effectively isolating all machinery on the false deck; applicable international	al
to lighter equipment only. [37]	
2.2.3 Raft Foundation (Double stage vibration isolation system) CC W 9 Adds NB/ RF All High, bes	st at
One or several pieces of machinery are mounted on an upper layer D Significantly to 2, 3 higher	۶r
of mounts supported by a raft (steel structure) which is further S Installation cost;	cies
supported on the null girder on a lower level set of mounts. This Can be 10%+ of	
reduces noise by creating an extra impedance barner to the cost of installed	
anging/generator: not applicable to 2 streke dissels due to high	
weight	
2.2.4 Acoustic Enclosures: CC S 9 Adds RF/NB 125 - 500 High	,
Structures designed to enclose a specific piece of machinery, D significantly to 2, 3	
absorbing airborne noise. This reduces the airborne transmission of installation cost; Used on	
energy to the hull and the generation of URN from the hull. [39]. can be 10%+ of vessels	
Typically used only with smaller diesels and gas turbines. cost of installed requiring very	
equipment low noise	
signatures	
Such as	
warsnips,	
research vessels after	
treatment of	

Treatment/Description	Advantage s/Benefits	Disadvantage	TRL	Cost Estimation	Applicability	Effect	Effect
	o, Dononito	o, on anongoo		Range	Ship Types	Range (Hz)	Reduction (dB)
					other noise paths.		
2.2.5 Active Cancellation: Reduction of machinery excitation of the hull structure by means of secondary excitation to cancel the original excitation. Uses sensors for measuring excitation, a device to read the sensor and actuators to produce counter phase excitation. Capital cost is high. [40]	CC	S D	6	Highly variable	NB	Effective at tuned frequencies	High Effective for discrete frequencies rather than overall noise levels
2.2.6 Spur/Helical Gear Noise Reduction Gear design can be used to optimize number of teeth & profile shift angle. This will optimize sound reduction due to teeth mashing lowering machinery noise. Also requires high quality manufacturing [41] [42]	F M	D	9	Increase in manufacture cost, can double gear cost (milspec)	NB	Effective mainly at gear meshing frequencies	Medium/ High
 2.2.7 Control of Flow Exhaust gases (Enabled by 2-stroke diesel Engine) Exhaust flow component designed to reduce noise produced by sudden gas expansion during the combustion/exhaust stroke of a 2-stroke diesel engine. [43] 	F	D	3	Unknown	NB 1, 4	Unknown	Low
2.2.8 Metallic Foam A porous material designed to be used in the tanks of diesel or water ballast tanks, to reduce underwater radiated noise. The material has open enhanced acoustical properties when saturated by liquids [44]	CC	N/A	6	Unknown	Unknown	Unknown	Unknown, claimed as High
2.2.9 Structural (Hull/Girder/Floor Thickening) The thickness of structural members are directly linked to URN mitigation. Rigid structure creates impedance mismatch and is particularly effective used with resilient mounts; added weight is also useful for noise transmission reduction [45]	CC	D S W F	9	Unknown	NB 2, 3	10 – 1000	Medium
2.2.10 Structural Damping Tiles The application of dampening tiles integrated into the structure of a vessel, absorbing vibration energy, resulting in a reduction of URN. [45]	CC	W D	9	\$50 – 150 per m²	NB/RF 2, 3	200+	High if treatment is extensive, best at higher frequencies
2.2.11 Acoustic Decoupling Coating Layer of rubber foam or polyethylene foam applied to the exterior of the vessels hull, designed to decrease noise radiation from machinery vibration energy. (most commonly applied to submarines)	F	M (Hard to control corrosion	7	\$250 – \$1000 per m ² plus engineering design and installation costs	NB/RF 2, 3	800+ 100 – 800	Unknown, claimed as High for higher frequencies

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Annex, page 10

Treatment/Description	Advantage s/Benefits	Disadvantage s/Challenges	TRL	Cost Estimation Percentage/	Applicability RF/ NB	Effect Frequency	Effect Noise
				Range	Ship Types	Range (Hz)	Reduction (dB)
[46]		between tiles & hull)					
2.3 Alternative fuel selection							
2.3.1 Fuel Cell	CC	D	7	High capital cost	NB	All	High
Produces electricity through chemical reaction, this is done by	E	Р					
converting hydrogen and oxygen to water. Significantly quieter than	W	S		Increase in fuel			
any combustion engine.	F			cost			
(The efficiency of fuel cells themselves are quite high however, when							
infrastructure & storage is taken into account compared to diesel or							
other methods, the efficiency decreases significantly) [47] [48] [49]							
2.3.2 Battery (Stored electrical energy, also supercapacitors)	E	S	9	High capital cost	NB/RF	All	High
Draws on stored energy provided by shore power or from integrated	F	W			2, 3		
electric power plant on ship. Batteries themselves are inherently					Applicable to		
silent removing all prime mover noise when in use. Low energy					vessels with		
density means can only be used for short voyages, or for portions of					short routes		
longer voyages in (e.g.) noise-sensitive areas. [50]					or highly		
					varying speed		
3.0 Hydrodynamic					promes		
3.1 Hull Treatments							
3.1.1 Underwater Hull Surface Maintenance	F	м	٥	Hull polishing	DE	A11	Low
Poor hull surface maintenance can lead to resistance increases	- -	141	3	cost depends on			LOW
This can cause the machinery load on machinery to increase and	-			shin size			
propeller RPM to travel at the same speeds, thus increasing LIRN				5110 5120			
Hull surface maintenance must be completed regularly to avoid this							
[51]							
3.1.2 Air Bubbler System (Masker): Air injection around the hull of	F	м	7 (in	20000 - 75000 +	NB	20-80	Hiah [78]
the vessel to reduce noise created by machinery, creates a blanket	-	D	comm	Pavback Period:	1, 2, 3	500+	
of air bubbles between the machinery noise and water, and uses			ercial	4 – 15 years			
tubing systems and an air compressor. Also has the effect of highly			ships)	[22]			
reducing marine growth on the hull, improving overall efficiency.			. ,				
Must be used while docked as well to reduce marine growth clogging							
tubing holes. Used by navies to reduce noise for detection stealth							
purposes. [29]							
3.1.3 Hull Air Lubrication:	F	D	8	Similar to 3.1.2	NB		High
Air lubrication systems (ALS) have been introduced by several		М			1, 2		-
shipbuilders to reduce skin friction resistance for power savings [80],							
[83]. It is probable that this will have similar effects to Masker							
systems on naval vessels.							

Treatment/Description	Advantage s/Benefits	Disadvantage s/Challenges	TRL	Cost Estimation Percentage/ Range	Applicability RF/ NB Ship Types	Effect Frequency Range (Hz)	Effect Noise Reduction (dB)
3.2 Hull Appendage/Design							
3.2.1 Efficient Hull Forms Hydrodynamically efficient hull forms will reduce power requirements and therefore both machinery and propulsor noise. Such hulls will also generally have good wake characteristics, increasing cavitation inception speeds. [52]	F	D	9	Unknown	NB All	ALL	Application dependent
3.2.2 Stern Flap/Wedge Small extensions from the lower transom. Modifies the stern wave produced by the vessel and reduces powering requirements, reducing hydrodynamic noise. Similar benefits will come from other stern flow modification appendages, such as hull vanes and interceptors. [53] [54]	F E	D	9	Unknown	NB/ RF 1, 2	ALL	Low
4.0 Other Mitigation Technologies							
4.1 Wind 4.1.1 Kite Sails Kites attached to the bow of a Merchant/commercial vessel, designed to create thrust that replaces power from conventional machinery and propeller thrust. [56]	F	D	8	Payback Period: 15+years [22]	NB/ RF 1, 4 Not suited to smaller vessels or to operations on short routes and fixed schedules, e.g. smaller ferries	ALL	Medium to High (Depending on speed reduction and primary propulsion source)
4.1.2 Flettner/Magnus Rotors Tall, smooth, rotating cylinders with an end plate at the top. Extruding from the main deck of the vessel. An external force with wind causes rotation creating thrust that replaces power from conventional machinery and propeller thrust. Similar to conventional sails in URN reduction. [57]	F	D S P	8	Payback Period: 15+years [22]	NB/ RF 1, 4 Not suited to smaller vessels or to operations on short routes and fixed schedules, e.g. smaller ferries	ALL	Medium to High (Depending on speed reduction and primary propulsion source)

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Treatment/Description	Advantage	Disadvantage	TRL	Cost Estimation	Applicability	Effect	Effect
	s/Benefits	s/Challenges		Percentage/	RF/ NB	Frequency	Noise
				Range	Ship Types	Range (Hz)	Reduction (dB)
4.1.3 Conventional Sails	F	D	9	Dependent on	NB	ALL	Medium to
As with kites and rotors, any form of sail assist can reduce		S		vessel and	3, 4		High
machinery power requirements and propeller noise.		Р		installation	Not suited to		(Depending on
					operations on		speed
					short routes		reduction and
					and fixed		primary
					schedules,		propulsion
					e.g. smaller		source)
					ferries		,
4.1.4 Cold Ironing (Shore Power)	E	S	9	\$1.5 m per berth,	NB/RF	<1000	Medium
Provision of higher power shore supplies to large vessels (cruise	F	W		\$400k per vessel	1		
ships, containers ships) can allow these vessels to turn off all	М			-	Also often		
generating equipment while in port, lowering URN while alongside.					used for		
[81]					smaller		
					vessels with		
					standard		
					home ports		

Predicting URN						
Prediction Method	Description	Comments	Software/Vendors (examples)	TRL		
1.0 Computational						
1.1 Propeller						
Empirical; e.g. Tip Vortex Cavitation Method	An approximate method based on numerical and experimental data. It is generally considered that tip cavitation produces the predominant noise produced by cavitation followed by sheet cavitation. [58], [84]	Semi-empirical methods require detailed knowledge on the appropriate empirical input parameters to be used which need to be scaled to the results of model or full scale tests. Uncertainty levels can be high.	Used by DNV and others for noise prediction	9		
Semi-empirical, e.g. Lifting Surface method\potential flow	Propeller Blades are analysed as lifting surfaces over which singularities such as the vortex are distributed over the surface to model the effects of blade loading/thickness. [65] [66] [67]. To perform this method detailed propeller geometry & wake distribution must be provided, pressure distribution calculations must be performed to produce lifting surfaces from the blade geometry. From here determination of sheet cavitation regions can take place, than calculations of sheet cavitation swept area can occur. This can then be converted to broad band noise levels using a conversion equation such a Brown's Formula [68], [88]	Incompressible flow methods such as lifting surface cannot capture viscous flow features such as boundary layers and vortices and have difficulty in modelling cavitation accurately.	PUF PROPCAV PROCAL	8		
Computational Fluid Dynamics	Tip Vortex cavitation can be predicted in many different ways using CFD. [58] The Reynolds stress turbulence model may be used for computation of propeller flow using FLUENT [59], transition-sensitive eddy-viscosity turbulence model to resolve the boundary transition layer effects [60], Commercial Reynolds Averaged Navier Stokes (RANS) solvers [61] [62], RANS solvers need to be paired with other methods to change the form of data calculated for example Detached-Eddy Simulations (DES) paired with the Spalart-Allmaras eddy viscosity model [63] or Direct Navier-Stokes simulations [64]. Conversion of tip vortex intensity into URN levels for high frequencies in particular requires similar approached to Lifting Surface methods using Brown's Formula or others as direct capture of tip vortex cavitation is difficult [89]	RANS codes consider viscous flow features in a more simplified way than LES (large eddy simulation) codes, giving lower accuracy in some cases but with less computational effort. None of these methods can be used other than by highly specialized personnel.	OpenFoam (Simple Foam RANS Solver) ANSYS (FLUENT) Star CCM+ ANSYS CFX ReFRESCO	7		
1.2 Machinery						
Empirical [69]	Empirical formulae have been derived for many airborne, duct-borne and structure-borne noise transmission paths, and can be combined into overall prediction methodologies.	These methodologies are mainly concerned with internal noise and require manipulation to be used for URN prediction.	DNVGL in-house software CABINS software from TNO	9		
Semi-empirical: Statistical Energy Analysis (SEA) [70]	SEA uses energy flow relationships to calculate the diffusion of acoustic and vibration energy through a structure before its propagation into the water. In the SEA method, a complex structure is considered as a system formed of coupled subsystems. Each subsystem represents a group of modes with	SEA methods are still reliant on empirical data for calibration, and the accuracy of predictions can be less than for empirical. Only	Designer-NOISE (Noise Control Engineering)	9 8		

Predicting URN					
Prediction Method	Description	Comments	Software/Vendors (examples)	TRL	
[71]	similar characteristics and a storage of energy. SEA predicts the average response of the structure, reducing the amount of calculation required.	specialized personnel can use method reliably.	SEAM (Cambridge Collaborative) Deltamarine		
Full Frequency Range Vibro-Acoustic Prediction	Utilizes statistical energy analysis (SEA), structural and acoustic finite element (FE), and boundary element (BE) solvers alone and combined in hybrid models for vibroacoustic response to machinery, flow-related and hydroacoustic inputs. FE and BE are used for low frequency ship response and URN prediction, hybrid FE/BE/SEA for higher frequency predictions, and SEA for high frequency predictions. Measured and empirical information can be incorporated as user-defined properties/characteristics.	The advanced SEA algorithms in these methods do not rely on empirical data. Considerable expertise in structural- acoustics is required to use these methods	VAOne (ESI Group) Wave6 (Dassault Systemes)		
Low Frequency Noise Prediction/Finite Element Methods [72]	The purpose of this method is to calculate URN caused by machinery noise similarly to the SEA method. The method requires a 3D CAD model converted to a Finite Element model. Various loads and analyses can take place to acquire results for radiated noise analysis. From here a wetted surface FE model and a Boundary Element (BE) code can be coupled to predict low Frequency URN		FE Software (similar to Ansys) Boundary element based code (Ex: AVAST)	8	
1.3 Entirety					
Noise propagation modelling [85], [86], [87]	 Various models can be accessed from the websites listed in the references using methods including parabolic equation, ray trace, normal modes and spectral integration. Some commercial codes have also been developed. 	All methods can only be exercised by specialized personnel.	RAM KRAKEN OASES dBSea [73]	9	
2.0 Model Scale					
Propeller cavitation tunnel	Cavitation tunnels model the propeller and in some cases the hull form immediately ahead of the propeller, reducing the pressure in the tunnel in accordance with scaling laws. Results predict cavitation inception speeds and the development of cavitation patterns. Tunnel tests can also be used to predict pressure pulses & cavitation noise. Noise levels from the model propeller are extrapolated to full scale using a variety of scaling rules. [78], [79]	Model scale cavitation testing has challenges for replication of wake field, blockage effects and others. Noise measurements are influenced by reverberation from tank walls, background noise and uncertain scaling laws. Open literature available regarding radiated noise full scale and model scale comparison and extrapolation can be found in [76].	Approximately 20 commercial model testing facilities have cavitation tunnels. Large scale tunnels are preferable to reduce scaling uncertainties. [74]	9	
Ship cavitation tank	Cavitation tanks extend the tunnel modelling approach by using whole ship models in a depressurized chamber. This allows for the creation of more accurate wake fields and flow patterns both upstream and downstream of the propeller, giving a more accurate prediction of cavitation. [76], [77]	While some modelling issues are improved compared to cavitation tunnel others become more challenging.	Only two depressurized tanks are in operation, in China and the Netherlands [75]	9	

APPENDIX 2

CITATION INDEX

[1] C. Audoly and C. Rousset, "Assessment of the solutions to reduce underwater radiated noise," Achieve Quieter oceans by shipping noise footprint reduction, WP: Practical Guidelines Task T5.3, Revision 1, September 2015.

[2] H. S. Han, K. H. Lee and S. H. Park, "Evaluation of the cavitation Inception Speed of the Ship Propeller using Acceleration on its Adjacent Structure," Journal of Mechanical Science and Technology, Vol. 30, Issue. 12, December 2016.

[3] J.P. Breslin and P. Andersen, "Hydrodynamics of Ship Propellers," Cambridge Ocean Technology Series, ISBN 0 521 41360, 1994.

[4] N. O. Hammer and R. F. McGinn, "Highly Skewed Propellers - Full Scale Vibration Test Results and Economic Considerations," The Ship Vibration Symposium, Arlington, October 1978.

[5] Renilson Marine Consulting Pty Ltd, "Reducing Underwater Noise Pollution From Large Commercial Vessels" The International Fund for Animal Welfare, March 2009.

[6] Perez Gomez, G. and Gonzalez Adalid, J, "Tip Loaded Propellers (CLT). Justification of their advantages over high skewed propellers using the New Momentum Theory," International Shipbuilding Progress, 1995.

[7] S. Gaggero, M. Viviani, D. Villa, D, Bertetta, C. Vaccaro, and S, Brizzolara, "Numerical and Experiment Analysis of a CLT Propeller Cavitation Behavior," Proceedings of the 8th International Symposium on Cavitation, CAV2012, Abstract. 84, Singapore, August 2012.

[8] A Hoorn, P.C. Van Kluijven, L. Kwakernaak, F. Zoetmulder, M. Ruigrok and K. de Bondt, "Contra-rotating propellers," Rotterdam Mainport University of Applied Science RMU.

[9] F. Mewis, "Pod drives – pros and cons," Hansa, 138/8, 2001.

[10] P. Anderson, S.V. Andersen, L. Bodger, J. Friesch and J.J Kappel, "Cavitation Considerations in the Design of Kappel Propellers," Proceedings of NCT'50 International Conference on Propeller Cavitation, University of Newcastle, April 2000.

[11] W. Laursen, "Advanced Propeller Designs Suit Slow Revving Engines," The Motor Ship Insight for Marine Technology Professionals, August 2012.

[12] Y. Inukai, "A Development of a Propeller with Backward Tip Raked Fin," Third International Symposium on Marine Propulsion, Tasmania, Australia, May 2013.

[13] F. Mewis, "The Efficiency of Pod Propulsion," 22nd International Conference Hadmar 2001, Varna, Bulgaria, October 2001.

[14] B. L. Southall and A. Scholik-Scholmer, "Potential Application of Vessel-Quieting Technology on Large Commercial Vessels," Final Report of the National Oceanic and Atmospheric Administration (NOAA) International Symposium, May 2007. [15] A.B Rudd, M.F Richlen, A.K. Stimpert and W.W.L. Au, "Underwater Sound Measurements of a High Speed Jet-Propelled Marine Craft: Implications for Large Whales," Pacific Science, Vol.69, No. 2, October 2014.

[16] R. Parchen, "Noise Production of Ship's Propellers and Waterjet Installations at Non-Cavitating Conditions," Acoustics Division/ Flow Acoustics.

[17] G. Zandervan, J. Holtrop, J. Windt and T.V. Terwisga, "On the Design and Analysis of Pre-Swirl Stators for Single and Twin Screw ships," Second International Symposium on Marine Propulsors, Hamburg, Germany, June 2011.

[18] F. Mewis and U. Hollenbach, "Special measures for Improving Propeller Efficiency," HSVA NewsWave the Hamburg Ship Model Basin Newsletter, January 2006.

[19] R. A. Topphol, "The Efficiency of a Mewis Duct in Waves," Norwegian University of Science and Technology, Department of Marine Technology. June 2013.

[20] C. Hao-peng, M. Cheng, C. Ke, Q. Zheng-fang and Y. Chen-jun, "An Integrative Design Method of Propeller and PBCF (Propeller Boss Cap Fins)," Third International Symposium on Marine Propulsion, Tasmaina, Australia, May 2013.

[21] H. R. Hansen, T. Dinham-Peren and T. Nojiri, "Model and Full Scale Evaluation of a Propeller Boss Cap Fin Device Fitted to an Aframax Tanker," Second International Symposium on Marine Propulsors, Hamburg, Germany, June 2011.

[22] R. Winkel, A. Van Den Bos and U. Weddige, "Study on Energy Efficiency Technologies for Ships," ECOFYS, Netherlands, June 2015.

[23] R. A. Topphol, "The Efficiency of a Mewis Duct in Waves," Norwegian University of Science and Technology, Department of Marine Technology. June 2013.

[24] "Promas," Rolls- Royce https://www.rolls-royce.com/products-and-services/marine/product-finder/propulsion-systems/propulsion-and-manoeuvring-system/promas-propulsion-and-manoeuvring-system.aspx#/

[25] J.T. Ligtelijn, "Advantages of different propellers for minimizing noise generation," Proceedings of the 3rd International Ship Noise and Vibration Conference, London, UK, September 2007.

[26] C. Liu, J. Wang and D. Wan, "The Numerical Investigation on Hydrodynamic Performance of Twisted Rudder during Self-Propulsion," State Key Laboratory of Ocean Engineering, School of Naval Architecture, Ocean and Civil Engineering, Shanghai Jiao Tong University, Collaborative Innovation Center for Advanced Ship and Deep-Sea Exploration, Shanghai China.

[27] H. Scheekluth, "Ship Design for Efficiency and Economy," Butterworth & Co, ISSBN 0-408-02790-9, 1987.

[28] C. M. Plumb and A. M. Kendrick, "Surface Ship Noise Reduction," Journal of Naval Engineering, Vol.26, No.3.

[29] "Ship's Silencing Program," Information sheet: 9.7, Surface Officer Warfare school.

[30] R.L. TOWNSIN, D.S. SPENCER, M. MOSAAD and G. PATIENCE, "Rough propeller penalties," Transactions of the Society of Naval Architects and Marine Engineers, 1985.

[31] 40. R. MUTTON, M. ATLAR, M. DOWNIE and C. ANDERSON, "The effect of foul release coating on propeller noise and cavitation," Proceedings of the International Conference on Advanced Marine Materials and Coatings, Royal Institution of Naval Architects, 2006.

[32] J. Carlton, Marine Propellers and Propulsion, 2nd ed. [EBOOK] Available: ebooks.

[33] HydroComp, "Singing Propellers," A HydroComp Technical Report, Report 138, July 2015.

[34] J. Spence, R. Fischer and M. Bathirian, "Review of existing and future potential treatments for reducing underwater sound from oil and gas and industry activities," 2007.

[35] V. Mrzlijak and T. Mrakovčić "Comparison of COGES and Diesel-Electric Ship Propulsion Systems," ISSN 0554-6397.

[36] 'Advantages and Disadvantages of the Stirling Engine', 2018. [Online]. Available: https://en.demotor.net/stirling-engine/advantages-disadvantages. [Accessed: 1- October- 2018].

[37] A. Nilsson, L. Kari, L. Feng and U. Carlsson, "Resilient Mounting of Engines," MWL, Department of Vehicle Engineering, KTH, 10044, Stockholm, Sweden.

[38] A. L. Tappu, A. K. Sen and M. M. Lele, "Design Sensitivity Analysis of Raft foundation for Marine Engines and Machinery in Warships" International Journal of Engineering Research and Applications (IJERA), Vol.3, Issue. 1, 2013.

[39] Christian Audoly and Enrico Rizzuto "Mitigation measures for controlling the ship underwater radiated noise, in the scope of AQUO Project" OCEANS, Genoa, May 2015.

[40] T. Basten and A. Berkhoff "Active Vibration Control for Underwater Signature Reduction of a Navy Ship" 17th International Congress on Sound and Vibration, Cairo 2010.

[41] P.Maior, "Numerical Research in Kisssoft for Noise Reduction in Spur Gears Transmissions," Science Bulletin of the University of Târgu Mureş, Vol.8, no.2, 2011. (2-MREF-1).

[42] B. R. Höhn, "Improvements on Noise Reduction and Efficiency of Gears," Meccanica, Vol. 45, Issue. 3, June 2010.

[43] Vigneshraj C T, Rajesh Kannan K and Vivek C, "Noise Reduction in Two Stroke Engine by Controlling the velocity of Exhaust Gas," International Journal of Advances in Engineering & Technology, Vol.9, Issue 4, p. 507-512, August 2016.

[44] J. García-Pelezá, J. Manuel Rego-Junco, and L. Sánchez-Ricart, "Reduction of Underwater Noise Radiated by Ships: Design of Metallic Foams for Diesel Tanks," IEEE Journal of Oceanic Engineering, Vol.43, No.2, April 2018.

[45] R. Salinas and A. Moreno, "Assessment of the solutions to reduce underwater radiated noise," Achieve Quieter oceans by shipping noise footprint reduction, WP: Practical Guidelines Task T5.3, Revision 1, September 2015.

[46] C. Audoly, Acoustic characterisation of anechoic or decoupling coatings taking into account the supporting hull. RINA warship conference. Naval submarines and UUV, Bath, UK, 29-30 June 2011.

[47] M. Krcum, L. Žižić and A. Gudelj, "Marine Applications for Fuel Cell Technology," University of Split, Faculty of Maritime Studies, Split, Croatia.

[48] C. Bourne, T. Nietsch, D. Griffiths and J. Morley, "Application of Fuel Cells in Surface Ships," ESTU F/03/00207/00/00, 2001.

[49] L. Van Biert, M. Godjevac, K. Visser and P. V. Aravind, "A Review of Fuel Cells for Maritime Applications," Journal of Power Sources, Vol. 327, P. 345 – 364, 2016.

[50] P. Dvorak, "New Battery Technology Encourages Large Hybrid Ships," Wind Power Engineering & Development, August, 2017.

[51] 'Evaluation of the Scientific Evidence to Inform the Probability of Effectiveness of Mitigation Measures in Reducing Shipping-Related Noise Levels Received by Southern Resident Killer Whales,' Canadian Science Advisory Secretariat, Science Advisory Report 2017/041, September 2017.

[52] R. Leaper, M. Renilson and C. Ryan "Reducing Underwater Noise from Large Commercial Ships: Current Status and Future Directions" Journal of Ocean Technology Vol 9, April 2014.

[53] D. Cumming, R. Pallard, E. Thornhill, D. Hally and M. Dervin, "Hydrodynamic Design of a Stern Flap Appendage for the Halifax Class Frigates," MARI-TECH 2006, Halifax, NS, June 2006.

[54] D. S. Cusanelli, "Hydrodynamic and Supportive Structure for Gated Ship Sterns – Amphibious Ship Stern Flap," 11th International Conference on Fast Sea Transportation FAST 2011, Honolulu, Hawaii, September 2011.

[55] C. Audoly, T. Gaggero, E. Baudin, T. Folegot, E. Rizzuto, R. S. Mullor, M. André, "Mitigation of Underwater Radiated Noise Related to Shipping and Its Impact on Marine Life: A Practical Approach Developed in the Scope of AQUO Project," IEEE Journal of Ocean Engineering, Vol.42, NO.2, April 2017.

[56] P.C. Shukla and K. Ghosh, "Revival of the Modern Wing Sails for the Propulsion of Commercial Ships," International Journal of Mathematical, Computational, Physical, Electrical and Computer Engineering, Vol.3, No.3, 2009.

[57] T. Suominen, "Rotor pilot project on M/S Estraden of Bore fleet," Bachelor of Marine Technology, Satakunta University of Applied Sciences, Finland, Pori, 2015.

[58] M. A. Ali, H. Peng, W. Qiu and R. Bensow, "Prediction of Propeller Tip Vortex using Openfoam," Proceedings of the 36th International Conference on Ocean, Offshore and Artic Engineering, OMAE 2017, Trondheim, Norway, July 2015.

[59] H. S. Rhee, and S. Joshi, "Computational validation for flow around a marine propeller using unstructured mesh based Navier-Stokes solver". JSME International Journal Series B Fluids and Thermal Engineering, Vol.48, Issue.5, 2005.

[60] X. Wang, and K. Walters "Computational analysis of marine-propeller performance using transition-sensitive turbulence modelling". Journal of fluids Engineering, ASME, Vol.134, Issue. 7, 2012.

[61] W. Qiu, H. Peng, S. Ni, L. Liu, and S. Mintu, "RANS computation of propeller tip vortex". International Journal of Offshore and Polar Engineering, Vol.23, Issue.1, 2013.

[62] G. Gaggeroa, G. Tania., M. Viviania, and F. Contib, "A study on the numerical prediction of propellers cavitating tip vortex". Journal of Ocean Engineering, Vol.92, 2014.

[63] R. Muscaria, A. D. Masciob, and R. Verziccoc, "Modeling of vortex dynamics in the wake of a marine propeller". Computers & Fluids, Vol.73, 2013.

[64] C. T. Hsiao, and G. L. Chahine, "Scaling of tip vortex cavitation inception for a marine open propeller". 27th Symposium on Naval Hydrodynamics, Seoul, the Republic of Korea, 2008.

[65] J. A. Azantyr, "A Computer Program for Calculation of Cavitation Extent and Excitation Forces for A Propeller Operating in Non-Uniform Velocity Field", International Shipbuilding Progress, Vol.26, No.276, 1977.

[66] J. E. Kerwin and C. S. Leel, "Prediction of Steady and Unsteady Marine Propeller Performance by Numerical Lifting Surface Theory", Trans. SNAME, Vol.86, 1978.

[67] J. A. Azantyr, "A Method for Analysis of Cavitating Marine Propellers in Non-Uniform Flow", International Shipbuilding Progress, Vol.41, No.427, p.223-242, 1994.

[68] S. Ekinci, F. Celik and M. Guner, "A Practical Noise Prediction Method for Cavitating Marine Propellers,".

[69] DNV-GL, "Underwater noise analysis," https://www.dnvgl.com/services/underwater-noiseanalysis-4705

[70] C. de Jong and Björn Peterson, "Resonant Underwater Radiation Revisited," Institute of Technical Acoustics, Technical University of Berlin, Einsteinufer 25, D-10587 Berlin, Germany.

[71] N. Vladimir, Ivan Lončar, Ivica Ančić and Ivo Senjanović, "Prediction of Noise Performance of RO-RO Passenger Ship by the Hybrid Statistical Energy Analysis," Pomorski zbornik Posebno izdanje, 29-45.

[72] L. Gilroy, "Predicting Very Low Frequency Underwater Radiated Noise for Full-Scale Ships," CFA/DAGA'04, Strasbourg, 2004.

[73] R. S. Pedersen and M. Keane, "Validation of dBSea, Underwater Noise Prediction Software. Pile Driving Focus," Journal of Shipping and Ocean Engineering – IN PRESS.

[74] Specialist Committee on Hydrodynamic Noise of the 28th ITTC "Guideline – Model-Scale Propeller Cavitation Noise Measurements" ITTC 2017.

[75] Catalogue of Towing Tank Facilities https://ittc.info/facilities/

[76] Bureau Veritas & DNVGL "Guidelines for Regulation of UW Noise from Commercial Shipping" Sonic Deliverable 5.4, November 2015.

[77] H. van Wijngaarden "Prediction of Propeller-Induced Hull-Pressure Fluctuations" PhD Thesis, Marin 2011.

[78] H. Neatby "Propeller Noise and Mitigation" DRDC presentation to CISMaRT, Halifax, November 2018.

[79] A. Vrijdag et. al. "Control of Propeller Cavitation in Operational Conditions" Journal of Marine Engineering and Technology, December 2014.

[80] M. Kawabuchi et. al. "CFD Predictions of Bubbly Flow around an Energy Saving Ship with Mitsubishi Air Lubrication System" MHI Technical Review Vol 48 No.1, March 2011.

[81] M. Sisson et. al. "The economics of Cold Ironing" Port Technology, edition 40.

[82] Wave 6 product https://www.3ds.com/products-services/simulia/products/wave6/

[83] S. Sindagi, R. Vijayakumar and B. Saxena "Frictional drag Reduction: Review and Numerical Investigation of Microbubble Drag Reduction in a Channel Flow" International Journal of Marine Engineering, April 2018.

[84] A. Raestad "Tip Vortex Index – an engineering approach to propeller noise prediction" The Naval Architect, July 1996.

[85] Ocean Acoustics Library (http://oalib.hlsresearch.com/);

[86] OALIB Acoustics Toolbox (http://oalib.hlsresearch.com/Modes/AcousticsToolbox/)

[87] Wang, L. S., Heaney, K., Pangerc, T., Theobald, P. D., Robinson, S. P., & Ainslie, M. A. "Review of underwater acoustic propagation models" National Physical Laboratory, Teddington, UK, 2014.

[88] N. A. Brown "Cavitation Noise Problems and Solutions" Proceedings of the International Symposium on Shipboard Acoustics, 1976.

[89] J. Bosschers "A Semi-Empirical Prediction Method for Broadband Hull-Pressure Fluctuations and Underwater Radiated Noise by Propeller Tip Vortex Cavitation", Journal of Marine Science and Engineering, 2018.