INTER-GOVERNMENTAL MARITIME CONSULTATIVE ORGANIZATION



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ASSEMBLY - 3rd session Agenda item 12

> APPROVAL OF THE RECOMMENDATIONS OF THE MARITIME SAFETY COMMITTEE ON STABILITY INFORMATION FOR SHIPS CARRYING GRAIN

> > RESOLUTION A.49(III) adopted on 18 October 1963

THE ASSEMBLY

TAKING NOTE of Article 16(i) of the Convention concerning the functions of the Assembly,

NOTING FURTHER Articles 22 and 30 of the Convention which set out the procedure for consideration and adoption of recommendations to members concerning maritime safety,

NOTING IN ADDITION that the recommendations of the Maritime Safety Committee were considered by the Council at its ninth session and transmitted to the Assembly,

BEARING IN MIND Regulation 12, Chapter VI - Carriage of Grain - of the International Convention for the Safety of Life at Sea, 1960, relating to the requirements for carriage of grain in specially constructed ships, and in particular paragraph (a) of that Regulation,

NOTING that many countries already use the requirements of Chapter VI of the International Convention for the Safety of Life at Sea, 1960, as an equivalent to the corresponding requirements of the International Convention for the Safety of Life at Sea, 1948, - 2 -

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HAVING CONSIDERED the recommendations of the Maritime Safety Committee on stability information for ships carrying grain,

DECIDES

- (1) to endorse the recommendations as set out in the Annex on stability information for ships carrying grain in accordance with Regulation 12, Chapter VI, of the International Convention for the Safety of Life at Sea, 1960;
- (2) to recommend that governments concerned give effect to these recommendations;
- (3) to recommend that governments, through the Secretariat, should exchange information on the action taken in this respect.

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ANNEX

RECOMMENDATIONS ON STABILITY INFORMATION FOR SHIPS CARRYING GRAIN

1. Regulation 12 of Chapter VI - Carriage of Grain - of the International Convention for the Safety of Life at Sea, 1960 relates to specially constructed ships with two or more vertical or sloping grain-tight longitudinal divisions suitably disposed to limit the effect of any transverse shift of grain.

2. In such ships, bulk grain may be carried without regard to special stowage conditions laid down for other ships (Regulations 4-11 of Chapter VI). Regulation 12 requires that the angle of heel caused by the shift of grain to a specified angle (8° if bulk grain is overstowed and 12° if not overstowed) after 2% sinkage by volume should not be greater than 5°. It further requires that masters of such ships should be provided with a grain loading plan and stability booklets approved by the Administration.

3. In order to assist masters of ships carrying grain in accordance with Regulation 12 to make the necessary calculations of the angle of heel to which the ship might list during the voyage and thus ensure that the ship will not exceed the prescribed angle of heel, the stability information supplied to masters, as required by Regulation 12(a)(iii), should contain information on heeling moments caused by shifting of grain cargo having different stowage factors. A.III/Res.49 ANNEX

4. These data should be given separately for each hold and information for the centre holds should cover both the following conditions: when the hold is over-stowed and when not over-stowed.

5. The heeling moments should be obtainable for various depths (or ullages) and stowage factors of grain loaded. Details should be given of the position of centre of gravity of cargo in relation to the depth of grain.

6. This information may be given in graphic, tabular, or any equivalent form. Appendices I and II show possible forms of presentation, but these are not intended to be exclusive.

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APPENDIX I

ADDITIONAL DATA FOR STABILITY BOOKLETS SUPPLIED TO MASTERS OF SHIPS CARRYING GRAIN, IN ACCORDANCE WITH REGULATION 12, CHAPTER VI, OF THE INTERNATIONAL CONVENTION FOR THE SAFETY OF LIFE AT SEA, 1960

(Possible form of presentation)

Additional data to be included for each cargo hold separately are shown on the two pro forma pages attached to this Appendix.

Explanatory notes on the preparation of these data

- 1. Each hold should be represented by a sketch outline of the transverse section.
- 2. Capacity and dimensions should be given for each hold.
- 3. A graph representing depth of grain, on loading and when levelled, in each hold against the heeling moment caused by the shift of a surface wedge of the grain from the horizontal of 12° after 2% sinkage by volume, should be shown for each compartment which may contain grain without overstow.
- 4. A further graph representing the depth of grain against the heeling moment should be shown for each centre hold when this hold is overstowed; in this case the heeling moments should be calculated after 2% sinkage by volume and a shift of the surface from horizontal of 8°.
- 5. Each graph should show the maximum heeling moment which will occur in the hold when the surface wedge assumed to shift is of grain stowing at 45, 55 and 65 cubic feet per ton, or of corresponding values in the metric system. It may be of some advantage to incorporate in the booklet another scale of cubic capacity against depth of grain for the compartments in each hold.
- 6. The graph should incorporate a scale of KG values (centre of gravity above keel) for both wing tank and centre hold against the depth of the grain on loading and when levelled.
- 7. For the purpose of these calculations it is proposed that any increase in the metacentric height due to a reduction in KG value when sinkage occurs in a partly filled hold or in a wing tank be disregarded.

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- 8. The reduction in KG value due to a sinkage of 2% by volume in each centre hold when full should be stated.
- 9. The units used should be specified for all data.

Instructions for the Master

- 1. Before commencing to load grain the Master should prepare a calculation of metacentric height for the projected voyage.
- 2. Deductions from the metacentric height should be made for the assumed loss of metacentric height due to the free surface effects of liquids in tanks.
- 3. The reduction in KG value for centre holds; when filled, due to a 2% sinkage by volume should be applied in calculating the metacentric height.
- 4. The sum of heeling moments should be combined from the individual moments of holds and wing tanks containing grain.
- 5. The displacement on departure and on arrival at the discharge port should be taken from the displacement and deadweight scale which must be included in the stability booklet.
- 6. The angles of heel for departure from the loading port and arrival at the discharge port should be determined from the following formula:

Tangent of angle of heel

= <u>Sum of heeling moments</u> displacement x GM (corrected)

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S.S. "Nonesuch" Hold No.2

Hold capacity	cu.ft.	or m ³
Hatch capacity	cu.ft.	or m ³
Maximum hold length	ft. or	m
Maximum hold width	ft. or	m
Maximum hold depth	ft. or	m
Reduction in KG value due to 2% sinkage of grain in full hold	ft. or	m



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Pro forma page



S.S. "Nonesuch" Hold No.3

Hold cap	pacity	1		cu.1	ĉt.	or	m ³
Hatch ca	apacit	су		cu.1	Et.	or	m ³
Maximum	hold	lengt	h	ft.	or	m	
Maximum	hold	width		ft.	or	771	
Maximum	hold	depth		ft.	or	m	
Reductio due to 2 grain ir	on in 2% sir 1 full	KG va nkage hold	luc of 	ft.	or	m	



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APPENDIX II

ADDITIONAL DATA FOR STABILITY BOOKLETS SUPPLIED TO MASTERS OF SHIPS CARRYING GRAIN, IN ACCORDANCE WITH REGULATION 12, CHAPTER VI, OF THE INTERNATIONAL CONVENTION FOR THE SAFETY OF LIFE AT SEA, 1960

(Possible form of presentation)

Explanatory notes

The following curves should be given for each hold; as shown on the pro forma page attached hereto:

- curves of grain capacity (in cu.ft. or m²);
- curve of position of centre of gravity above base line (in feet or metres);
- curves of heeling moment (in feet⁴ or metres⁴) due to shift of grain which, after application of a stowage factor gives the heeling moment in feet/tons or metres/tons.

These curves should be shown against the ullage below the top of the hatch at the mid-length on the centre line (in feet or metres) on loading and when levelled.

The curve of heeling moments should be estimated assuming a 2% sinkage by volume followed by a shift of grain surface to an angle of 12° with the horizontal for cases where there is no overstowing. In cases where over-stowing is used (assumed shift is 8°) the heeling moment can be taken as 70% of that given for the 12° shift.

To ensure that the possible angle of heel due to shift of grain for a particular loading does not exceed that prescribed (5°) , the usual trim calculation is made and the longitudinal position of the vessel's centre of gravity is obtained, together with the transverse metracentric height corrected for effect of liquid free surface (GM_{c}) .

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The angle of heel (Θ) will be determined from the following formula:

$$\operatorname{Fan} \Theta = \frac{M}{\Delta \times \operatorname{GM}_{c} \times S}$$

(Tan Θ must be less than 0.0875 to satisfy the requirements of the Convention)

or alternatively:

$$\Theta^{\circ} = \frac{57.3 \times M}{\Delta \times GM_{c} \times \beta}$$
 (Θ must be less than 5° to
satisfy the requirements of
the Convention)

WHERE:

 $M = \text{total grain heeling moment in feet}^4$ $\Delta = \text{vessel's displacement in tons}$ $GM_c = \text{transverse metacentric height in feet} (corrected for liquid free surface)$ f = (stowage factor) in cubic feet/ton.A sample calculation is given on the following pages. EXAMPLE

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LOADED DEPARTURE CONDITION WITH GRAIN CARGO HOMOGENEOUSLY STOWED AT 46 CUBIC FEET/TON IN Nos. 2, 3, 4, 5 and 6 HOLDS, ALL HOLDS BEING SLACK. THE ULLAGES FOR EACH HOLD ARE LISTED BELOW. VESSEL'S DISPLACEMENT: 21,059 TONS

Metacentre above the base line KM = 2,842 feet

(1) CARGO WEIGHT, POSITION OF CENTRE OF GRAVITY ABOVE BASE LINE AND HEELING MOMENT

Hold No.	Ullage (in fect)	Capacity in cubic feet or metres from curves	Position of centre of gravity above base	Vertical moments ft ⁴	Heeling moments (curves) ft ⁴	REMARK S
ı.	-	-	-	-	-	Empty
2	0.6"	146,900	24.77	3,638,713	21,000	No over-stowing
3	6.0"	141,800	22.36	3,170,648	57,000	17 11
4	9.0"	133,200	20.97	2,793,204	101,000	11 11
5	10.6"	129,600	20.54	2,661,984	128,000	11 11
6	10.6"	144,000	24.23	3,489,120	19,000	11 . 11
		695,500	22.65	15,753,669	M=326,000	

CARGO WEIGHT = $\frac{695,500}{1000}$ = 15,120 tons

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ΙΤΕΜ	Tons	Position of centre of gravity above base	Vertical moments tons-feet
Light ship	5,259	26.00	136,734
Fuel, FW, Stores, etc.	680	22.80	15,504
Grain cargo (see 1)	15,120	22.65	342,468
DISPLACEMENT	21,059	23.49	494,706
Transverse metacentre above base Transverse metacentric height (uncorrected) Liquid free surface correction Transverse GM (corrected for liquid free surface)		28.42 + 4.93 - 0.14 + 4.79	

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ESTIMATED ANGLE OF HEEL $\theta^{\circ} = \frac{57.3 \times 326,000}{21059 \times 4.79 \times 46} = \frac{4.1^{\circ}}{---}$ (less than 5°, therefore satisfies the requirements of the Convention)

PRO FORMA PAGE

HOLD NO. 2

(67'3" LONG)



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